

... , 15, 49005, ... ; e-mail: L_anjyta@bigmir.net

25645.166 – 2004 «

(300-700)
2 (1,07 · 10⁻¹² / 3 , 1,22 · 10⁻¹⁰ / 3).

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300 ()

25645.166 – 2004

(300-700)
2 (1,07 · 10⁻¹² / 3 , 1,22 · 10⁻¹⁰ / 3).

Improving the quality of Earth remote sensing systems is largely due to the development of spacecraft motion control algorithms. A new control problem is to maintain given orbit parameters over a long period of time. To do this, it is proposed to constantly (continuously or discretely) counteract disturbing actions on the spacecraft. The capabilities of modern electrojet engines make it possible to counteract significant aerodynamic actions. This, in its turn, opens up possibilities of reducing the range of working orbits for remote sensing spacecraft to unconventionally low (very low or superlow) orbits of altitude about 300 km. Such superlow orbits for remote sensing spacecraft have a number of advantages.

In low Earth orbits, one of the main disturbing actions is aerodynamic drag. Its estimation is necessary at the preliminary design stage of spacecraft power supply systems when developing requirements for disturbance-

counteracting engines. The purpose of this paper is to estimate the possible atmospheric density, which would allow one to quickly conduct pre-design calculations of the aerodynamic drag on the spacecraft for given orbital flight conditions. The density was estimated using the Standard GOST R 25645.166 – 2004, “The Earth’s Upper Atmosphere. Density Model for Ballistic Support of Satellite Flights,” depending on the altitude and a fixed level of solar activity. In doing so, the effect of the following factors on the atmospheric density was considered: the daily effect, the semi-annual effect, and the effect of solar and geomagnetic activity. The coefficients that describe the effect of these factors were estimated at altitudes of 300 to 700 km, and the conditions under which these coefficients and the atmospheric density take extreme (maximum/minimum) were determined. As an example, it was shown that at an altitude of 300 km, the density can theoretically vary by more than two orders of magnitude (from 1.07e-12 kg/m³ to 1.22e-10 kg/m³). The results presented in this paper allow one to quickly estimate the possible range of the aerodynamic drag on the spacecraft.

Keywords: statistical criterion, dispersion, principal components method, solid-propellant engine, covariation matrix.

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 25645.166-2004 [7], -
 [7] -

$$\rho = \rho_H K_0 (1 + K_1 + K_2 + K_3 + K_4),$$

ρ_H – ; K_0 –
 F_{81} (

$$F_{10.7} \quad (81) \quad F_0 ($$

[7]); K_1 – ,

$K_2 -$, $K_3 -$, $F_{10.7}$ F_{81} ;
 $K_4 -$, $(\dots), 1 \dots = 10^{22} / (2 \dots)$ [8].

$$K_0 = \dots [7]$$

75 ... 250 ... 25 ...)

$$K_0 = 1 + \frac{F_{81} - F_0}{F_0} \sum_{i=0}^4 l_i h^i$$

$l_i (i = 0, 1, \dots, 4) -$

$h -$

$$\frac{(F_{81})}{(F_0)} K_0 = \dots [7]$$

$$|F_{81} - F_0| = 12,5 \dots (25 \dots - \dots) [7]$$

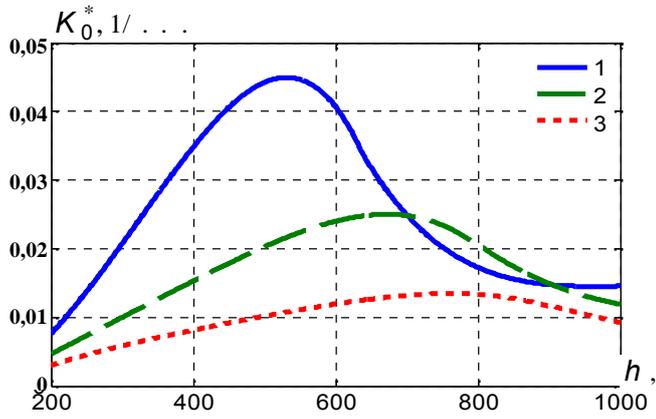
$$K_0 = 1 + K_0^* (F_{81} - F_0)$$

$$K_0^* = \frac{1}{F_0} \sum_{i=0}^4 l_i h^i$$

K_0^*

$F_0 = 150 \dots, 3 -$

$F_0 = 75 \dots, 2 -$
 $F_0 = 250 \dots$



. 1

, F_{81} F_0
 $h_{эксп}$

532, $\max(K_0^*) = 0,045$ 1/...

($F_0 = 150$... $h_{эксп} \approx 672$ K_0

$\max(K_0^*) = 0,025$ 1/... ; $F_0 = 250$... $h_{эксп} \approx 763$

$\max(K_0^*) = 0,0134$ 1/...). K_0 -

1.

. 1

	$F_0 = 75$...		$F_0 = 150$...		$F_0 = 250$...	
	$\min(K_0)$	$\max(K_0)$	$\min(K_0)$	$\max(K_0)$	$\min(K_0)$	$\max(K_0)$
$h = 300$	0,741	1,259	0,875	1,125	0,927	1,073
$h = 400$	0,565	1,435	0,809	1,191	0,898	1,102
$h = 500$	0,447	1,553	0,747	1,253	0,873	1,127
$h = 600$	0,492	1,508	0,700	1,300	0,851	1,149
$h = 700$	0,689	1,311	0,690	1,310	0,835	1,165

. K_1 ,
 , -
 -
 . K_1 -

$$K_1 = \sum_{i=0}^4 c_i h^i \cdot \cos^{n_0+n_1h+n_2h^2} \varphi/2, \quad \max(K_1) = K_1^* = \sum_{i=0}^4 c_i h^i,$$

c_i ($i = 0, 1, \dots, 4$), n_j ($i = 0, 1, 2$) - [7]; φ -

K_1 ,

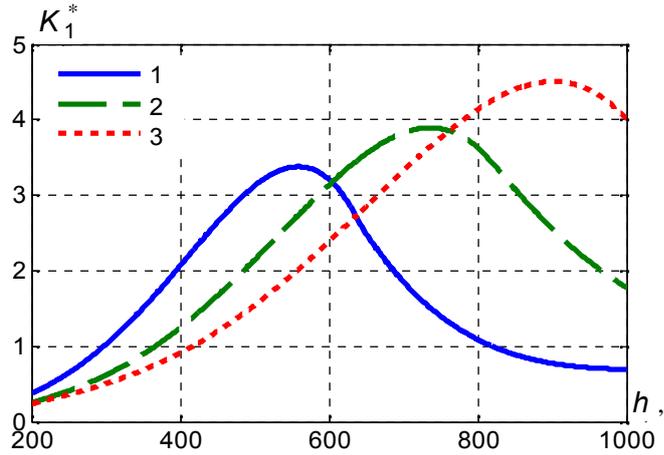
[9].

F_0

2

K_1^*

$F_0=75 \dots \max(K_1^*)=3,377$ 559 ; $F_0=150 \dots$
 $\max(K_1^*)=3,893$ 736 ; $F_0=250 \dots \max(K_1^*)=4,506$
 902 .



.2

K_1

0

K_1^*

K_1

2.

.2

	$F_0 = 75 \dots$		$F_0 = 150 \dots$		$F_0 = 250 \dots$	
	$\min(K_1)$	$\max(K_1)$	$\min(K_1)$	$\max(K_1)$	$\min(K_1)$	$\max(K_1)$
$h = 300$	0,000	1,022	0,000	0,618	0,000	0,506
$h = 400$		2,070		1,245		0,911
$h = 500$		3,124		2,147		1,543
$h = 600$		3,212		3,136		2,385
$h = 700$		1,855		3,826		3,322

700

K_1

4

$F_0=150 \dots$

K_2 ,

$$K_2 = \left(\sum_{i=0}^4 d_i h^i \right) \cdot A(d); \quad A(d) = \sum_{j=0}^8 A_j d^j,$$

d_i ($i = 0, 1, \dots, 4$) –

[7]; $A(d)$ –

;

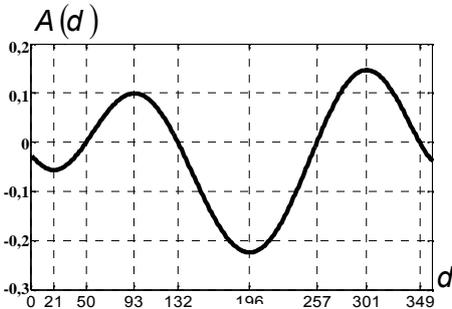
A_j ($j = 0, 1, \dots, 8$) –

K_2

[7].

$A(d)$

3.



.3

(50-, 132-, ...).

196-

15

(16

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(28

– 301-

27

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K_2

3.

.3

	$F_0 = 75 \dots$		$F_0 = 150 \dots$		$F_0 = 250 \dots$	
	$\min(K_2)$	$\max(K_2)$	$\min(K_2)$	$\max(K_2)$	$\min(K_2)$	$\max(K_2)$
$h = 300$	-0,291	0,190	-0,267	0,174	-0,263	0,172
$h = 400$	-0,387	0,253	-0,335	0,219	-0,320	0,209
$h = 500$	-0,462	0,302	-0,398	0,260	-0,368	0,240
$h = 600$	-0,513	0,335	-0,452	0,296	-0,409	0,267
$h = 700$	-0,539	0,352	-0,498	0,325	-0,444	0,290

($F_{10,7}$ F_{81}).

[7]

$F_{10,7}$ F_{81}

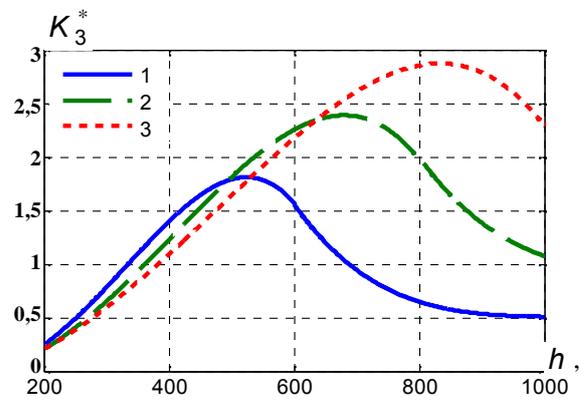
$$K_3 = \frac{F_{10,7} - F_{81}}{F_{81} + |F_{10,7} - F_{81}|} \cdot K_3^*, \quad K_3^* = \sum_{i=0}^4 b_i h^i,$$

b_i ($i = 0, 1, \dots, 4$) –

[7].

$$F_{81} = \frac{\sum_{i=-80}^0 F_i W_i}{\sum_{i=-80}^0 W_i}, \quad W_i = 1 + \frac{0,5i}{80},$$

$F_i - F_{10,7} \quad i \quad (i = 0, \dots, 80)$
 $F_{81}, \quad i = -80 - \dots, \dots$
) [7].
 81 $(F_{10,7} = F_{81}), \quad K_3 = 0.$
 $F_{10,7} = 2F_{81},$
 $K_3 = 0,5K_3^*.$



. 4

K_3
)
 80
)

$$F_{81} = \frac{F_{80} \sum_{i=-80}^1 W_i + F_{10,7} \cdot 1}{\sum_{i=-80}^0 W_i},$$

$F_{80} - F_{10,7} \quad F_{10,7} = F_{80} \pm f, \quad f - \ll \gg$
 80

$$F_{81} = \frac{F_{80} \left(\sum_{i=-80}^0 W_i - 1 \right) + F_{80} \pm f}{\sum_{i=-80}^0 W_i} = \frac{F_{80} \sum_{i=-80}^0 W_i \pm f}{\sum_{i=-80}^0 W_i} = F_{80} \pm \frac{f}{\sum_{i=-80}^0 W_i}.$$

$$\sum_{i=-80}^0 W_i = 60 \frac{3}{4}.$$

$$K_3^*, F_{80}, F_{10,7},$$

$$K_3^* = \frac{K_3}{\beta} = \frac{\pm 60 \frac{3}{4} \mp 1}{\frac{F_{80}}{f} \cdot 60 \frac{3}{4} \pm 1 + \left| \pm 60 \frac{3}{4} \mp 1 \right|}$$

$$K_3^*,$$

80

$$K_3^* \uparrow ($$

$$K_3^* \downarrow),$$

$$K_3^* \uparrow = \frac{239}{243} \cdot \frac{f}{F_{80} + f} \quad K_3^* \downarrow = -\frac{239 \cdot f}{243 \cdot F_{80} + 235 \cdot f}$$

$F_{10,7}$

50 ... 300 ... [9].

5

$$K_3^* \uparrow$$

$$K_3^* \downarrow$$

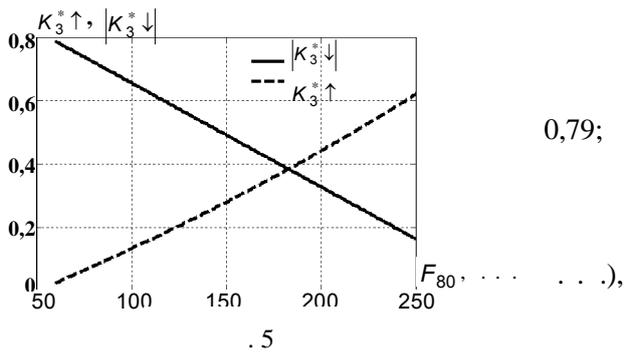
F_{80}

60 ... 250 ...

$$(\quad , \quad F_{80} + f = \max(F_{10,7}) = 300 \quad \dots$$

$$K_3^* \uparrow \quad F_{80} - f = \min(F_{10,7}) = 50 \quad \dots \quad K_3^* \downarrow).$$

($F_{80} = 60 \dots$)



(300 ...),

$$K_3^*$$

0,79;

($F_{80} = 250 \dots$)

(50

$$K_3^*$$

0,62.

$$K_3$$

(...) 300 ...

$$50$$

4.

	$F_0 = 75 \dots$		$F_0 = 150 \dots$		$F_0 = 250 \dots$	
	$\min(K_3)$	$\max(K_3)$	$\min(K_3)$	$\max(K_3)$	$\min(K_3)$	$\max(K_3)$
$h = 300$	-0,196	0,587	-0,260	0,325	-0,264	0,099
$h = 400$	-0,349	1,047	-0,490	0,613	-0,484	0,182
$h = 500$	-0,448	1,343	-0,724	0,905	-0,729	0,273
$h = 600$	-0,392	1,177	-0,901	1,127	-0,966	0,362
$h = 700$	-0,237	0,710	-0,952	1,189	-1,161	0,435

$K_4,$

$$K_4 = \sum_{i=0}^4 e_i h^i \cdot (e_5 + e_6 K_p + e_7 K_p^2 + e_8 K_p^3),$$

$e_i (i = 1, \dots, 8) -$ [7]; $K_p -$

[7]

K_4

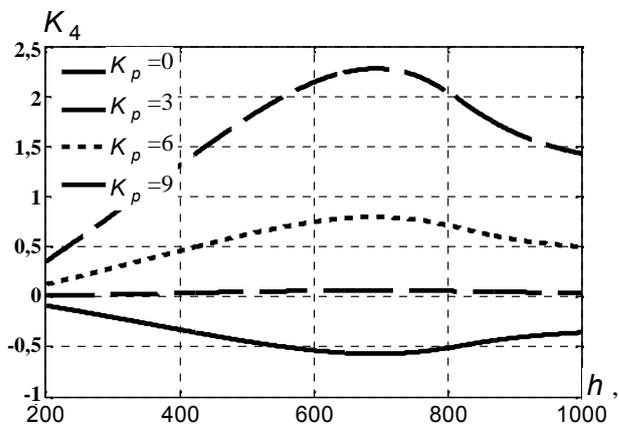
/ $K_p / k_p,$

/ A_p / a_p

K_4

$F_0 = 150 \dots$

$K_p.$



.6

K_4

$K_p).$ $K_p \approx 3$ $K_4 \approx 0.$

K_4 [7]

$K_p = 9,$

K_p

K_4 (5).

	$F_0 = 75 \dots$	$F_0 = 150 \dots$	$F_0 = 250 \dots$
$\max(K_4)$	3,114	2,278	1,939
$\min(K_4)$	-0,723	-0,570	-0,506
$h_{\text{экрп}}$	538	694	832

K_4 6.

	$F_0 = 75 \dots$		$F_0 = 150 \dots$		$F_0 = 250 \dots$	
	$\min(K_4)$	$\max(K_4)$	$\min(K_4)$	$\max(K_4)$	$\min(K_4)$	$\max(K_4)$
$h = 300$	-0,334	1,439	-0,205	0,819	-0,158	0,607
$h = 400$	-0,553	2,383	-0,328	1,310	-0,244	0,936
$h = 500$	-0,706	3,045	-0,445	1,778	-0,325	1,247
$h = 600$	-0,667	2,875	-0,535	2,140	-0,397	1,523
$h = 700$	-0,466	2,010	-0,570	2,277	-0,456	1,749

$K_i (i = 0, 1, \dots, 4)$

K_1 ,

K_1^*

$(F_0(F_{81}))$

2.

K_1

0

K_1^*

K_2, K_3, K_4

K_2 ,

196-

(16

15

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301-

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K_3 ,

K_3 ,

(

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(

81

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K_3 .

K_4 ,

$K_p = 0$ $K_p = 9$ (7); $K_p \approx 0,3333$

$K_4 = 0$.

K_3

$F_{10..7} = 300 \dots F_{81} = 60 \dots$,

($F_{10..7} = 50 \dots F_{81} = 250 \dots$).

$K_p = 9$ [10].

K_0

(F_{81}) [7]

(F_0). $K_0 = 1$

$F_{81} = F_0$; $|F_{81} - F_0| = 12,5 \dots$

K_i

()

7

$K = K_0(1 + K_1 + K_2 + K_3 + K_4)$

300

	$\rho_H, / ^3$	K_{\min}	K_{\max}	$\rho_H K_{\min}, / ^3$	$\rho_H K_{\max}, / ^3$
$F_0 = 75 \dots$	8,10e-12	0,1326	5,3356	1,07 -12	4,32 -11
$F_0 = 150 \dots$	2,27e-11	0,2345	3,3030	5,32 -12	7,50 -11
$F_0 = 250 \dots$	4,76e-11	0,2920	2,5580	1,39 -11	1,22 -10

K_i ,

K_i (300–700)

K_i

300

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24.05.2019,
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