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The Institute of technical mechanics of the National Academy of Sciences has developed technology for obtaining fine-dispersed media: solid + water method of cavitation pulse processing of solids. Timely and objective analysis of influence of modes of cavitation pulse plant and its design parameters on the crushing efficiency of the solid particles and the spectrum of their sizes is an urgent task. The purpose of this article is to analyze the possible ways and methods for rapid determination of the particle size, the choice of the most convenient way for use in our environment and adapting it to the conditions of the researches of cavitation - pulse technology.

Consumption of powders and their mixtures is becoming more common. Need them metallurgy, medicine, paint industry etc. Increasing competition among manufacturers of various products makes increasing demands

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on the stability of technological processes of their production, which in turn dictates the increase of requirements to reliability of data on the characteristics of the components used. Simultaneously with the increase of requirements to quality of the composition of fine materials, growing demands on the quality and efficiency definition of this structure. It is clear, applies to the granulometric composition of the components. It is known that the particle size distribution of powders is a crucial and often determining factor in the manufacturability of their application.

Keywords: *undercarriage parts perspective of the freight car, the dynamic quality of the crew, the stability of motion, recommendations for improving VSC.*

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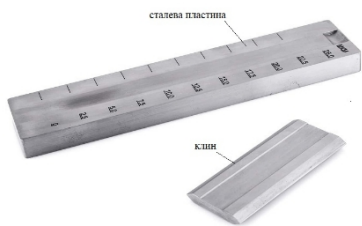
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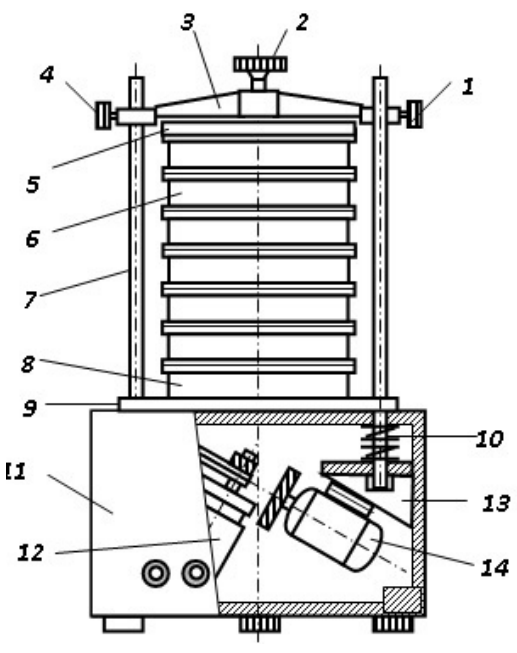
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(30 – 70)

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- 1, 2, 4 - кріпильні гвинти;
- 3 - траверса;
- 5 - кришка;
- 6 - набір сит;
- 7 - стійки;
- 8 - підон;
- 9 - опора;
- 10 - пружини;
- 11 - корпус;
- 12, 14 - електродвигуни;
- 13 - кронштейни.

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 90 % , 50 30 % , -
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 125 , 100 : 500 , 400 , 315 , 250 , 200 , 160 ,
 , 71 , 50 , 40 .

$$G = (n+1) \cdot G, \quad (1)$$

$G -$ () ; $n -$
 $G -$
 (, , ,)
 " " - R .
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 ()
 $2 \dots n$ $R(i) -$ $i -$. ($R(i), i = 1,$
 " " , , -
 , -

(, - R (i), i -) -

$$R (i) = R (i) - R (i-1). \quad (2)$$

G .

$$R_{\%} (i) = \frac{R (i) - R (i-1)}{G} \cdot 100\%, \quad (3)$$

R_{\%} (i) - i-

$$R_{\%} (i) = \frac{G - R (i)}{G} \cdot 100\%, \quad (4)$$

R_{\%} (i) - ; G - i-

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1. - R (i) i + 1 (i -)

2. i . i + 1 -

3. , -

4. i + 1 40

5. .

6. $- R(i)$ -
 $- G$. -
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G , $- R(i)$. $R(i) = R(i) - R(i-1)$. -
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Excel
 1 - 4 3 - 8 -

- , (3) (4). -

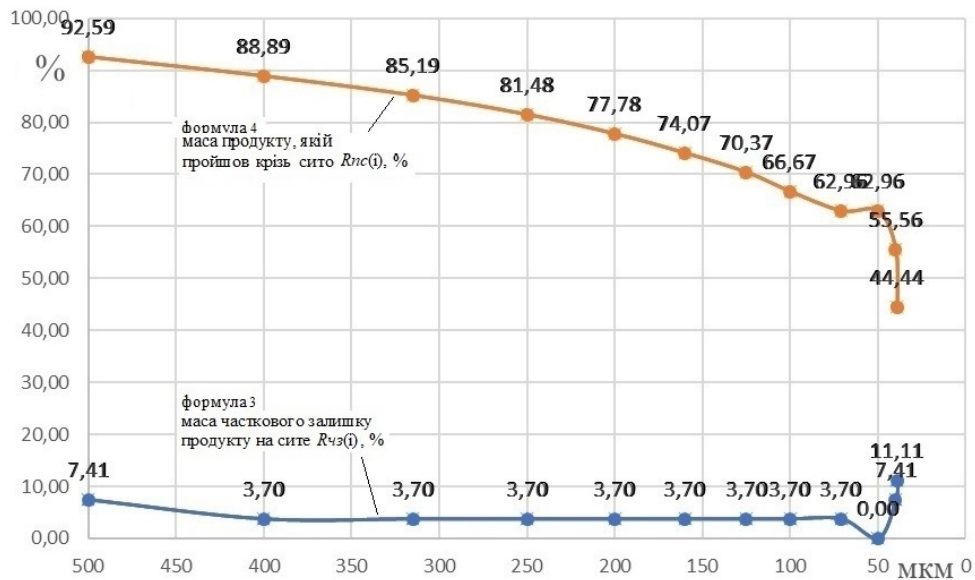
. 1. 54 % 46 % , -

МКМ	500	400	315	250	200	160	125	100	71	50	40	<40
$R_{\text{из}}(i)$, ГР	4,00	6,00	8,00	10,00	12,00	14,00	16,00	18,00	20,00	20,00	24,00	30,00
$R_{\text{из}}(i)$, %	7,41	11,11	14,81	18,52	22,22	25,93	29,63	33,33	37,04	37,04	44,44	55,56
$R_{\text{чз}}(i)$, %	7,41	3,70	3,70	3,70	3,70	3,70	3,70	3,70	3,70	0,00	7,41	11,11

. 2. 54 % 46 % , -

МКМ	500	400	315	250	200	160	125	100	71	50	40	<40
$R_{\text{из}}(i)$, ГР	4,00	6,00	8,00	10,00	12,00	14,00	16,00	18,00	20,00	20,00	24,00	30,00
$R_{\text{нч}}(i)$, ГР	50,00	48,00	46,00	44,00	42,00	40,00	38,00	36,00	34,00	34,00	30,00	24,00
$R_{\text{нч}}(i)$, %	92,59	88,89	85,19	81,48	77,78	74,07	70,37	66,67	62,96	62,96	55,56	44,44

. 3
 54 % 46 % , -
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. 3 – 54 %
46 % , (3) (4)

. 3. 60 % 40 % , -

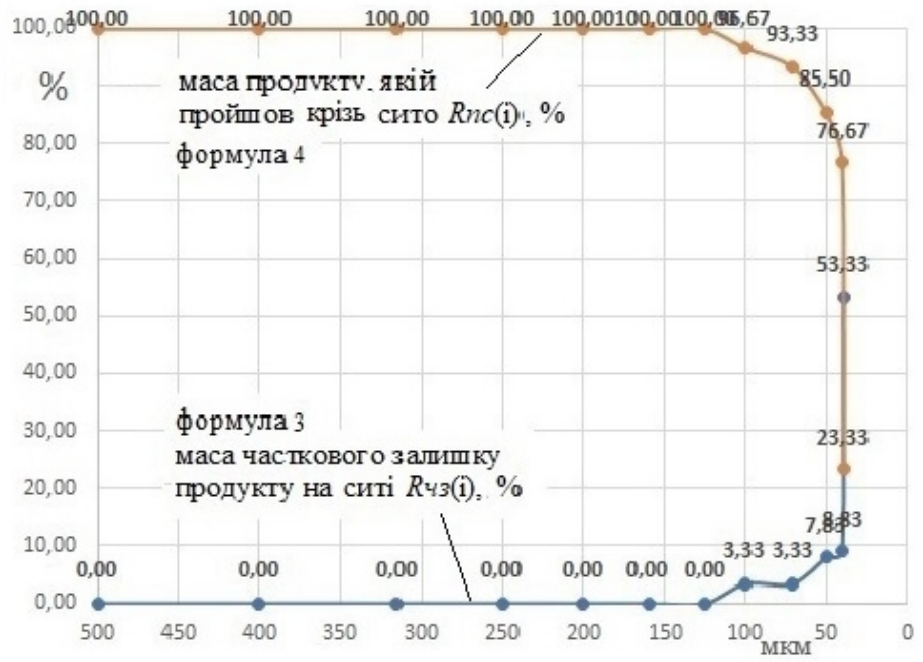
МКМ	500	400	315	250	200	160	125	100	71	50	40	<40
$R_{nc}(i), \text{ гр}$	0,00	0,00	0,00	0,00	0,00	0,00	0,00	2,00	4,00	8,70	14,00	46,00
$R_{nc}(i), \%$	0,00	0,00	0,00	0,00	0,00	0,00	0,00	3,33	6,67	14,50	23,33	76,67
$R_{чз}(i), \%$	0,00	0,00	0,00	0,00	0,00	0,00	0,00	3,33	3,33	7,83	8,83	53,33

. 4. 60 % 40 % , -

МКМ	500	400	315	250	200	160	125	100	71	50	40	<40
$R_{nc}(i), \text{ гр}$	0,00	0,00	0,00	0,00	0,00	0,00	0,00	2,00	4,00	8,70	14,00	46,00
$R_{nc}(i), \text{ гр}$	60,00	60,00	60,00	60,00	60,00	60,00	60,00	58,00	56,00	51,30	46,00	14,00
$R_{nc}(i), \%$	100,00	100,00	100,00	100,00	100,00	100,00	100,00	96,67	93,33	85,50	76,67	23,33

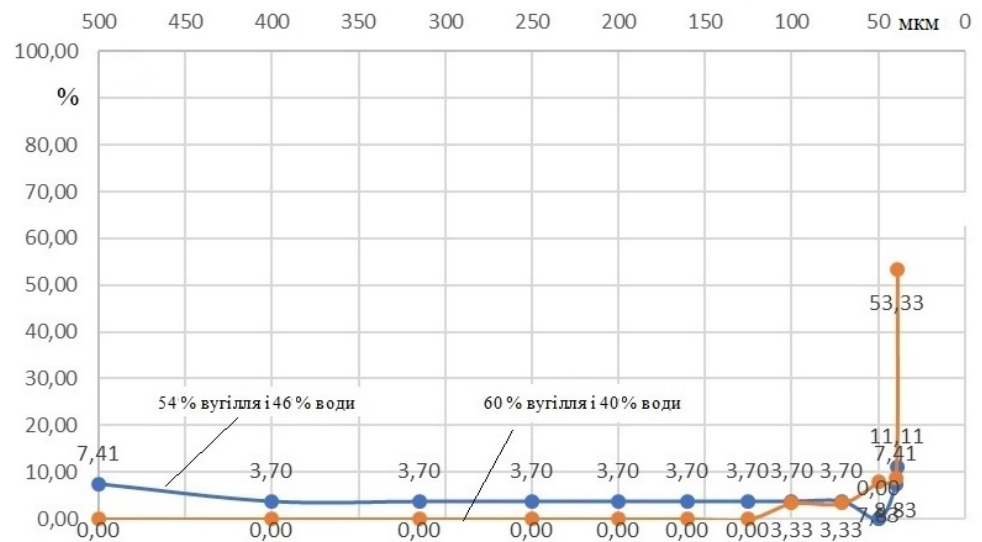
4 60 % 40 % , -

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. 4 – 40 % , (3) (4) 60 %

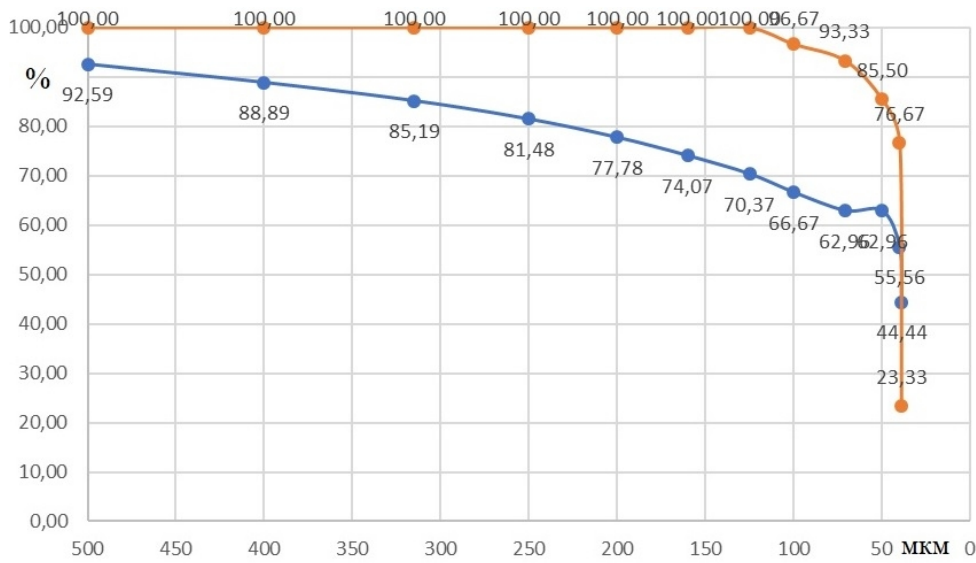
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. 5 -

70 % 30 % ,

MKM	500	400	315	250	200	160	125	100	71	50	40	<40
$R_{\text{пз}}(i), \text{ГР}$	6,00	8,00	16,00	18,00	24,00	25,00	26,00	29,00	30,00	32,00	34,00	36,00
$R_{\text{пз}}(i), \%$	8,57	11,43	22,86	25,71	34,29	35,71	37,14	41,43	42,86	45,71	48,57	51,43
$R_{\text{чз}}(i), \%$	8,57	2,86	11,43	2,86	8,57	1,43	1,43	4,29	1,43	2,86	2,86	51,43

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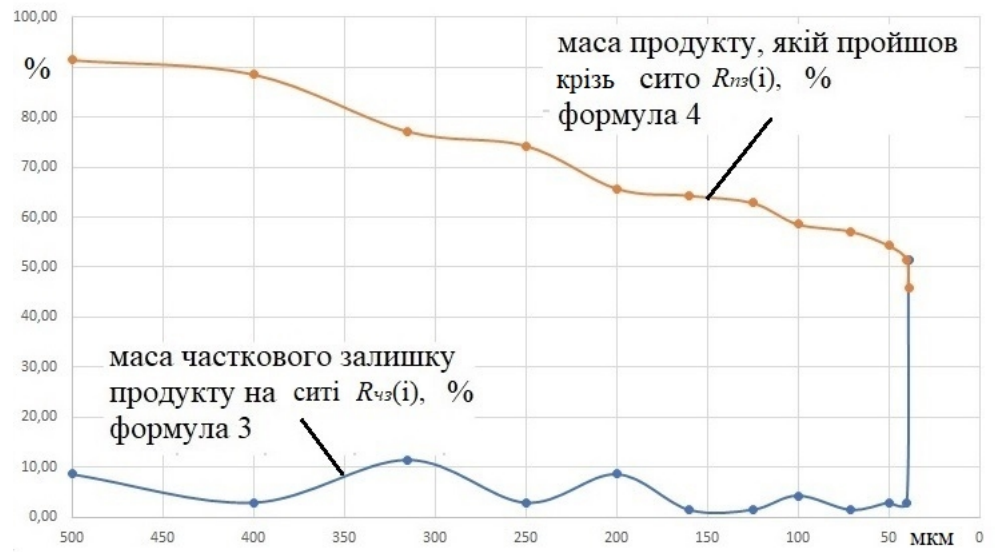
70 % 30 % ,

MKM	500	400	315	250	200	160	125	100	71	50	40	<40
$R_{\text{пз}}(i), \text{ГР}$	6,00	8,00	16,00	18,00	24,00	25,00	26,00	29,00	30,00	32,00	34,00	38,00
$R_{\text{пч}}(i), \text{ГР}$	64,00	62,00	54,00	52,00	46,00	45,00	44,00	41,00	40,00	38,00	36,00	40,00
$R_{\text{пч}}(i), \%$	91,43	88,57	77,14	74,29	65,71	64,29	62,86	58,57	57,14	54,29	51,43	45,71

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70 % 30 % ,

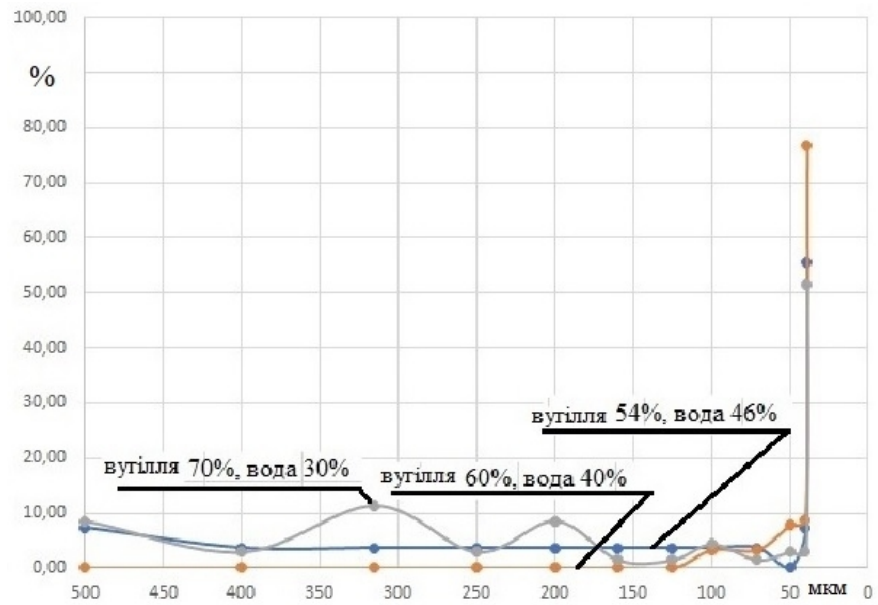
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. 7 – 70 % 30 % , (3) (4)

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(3).

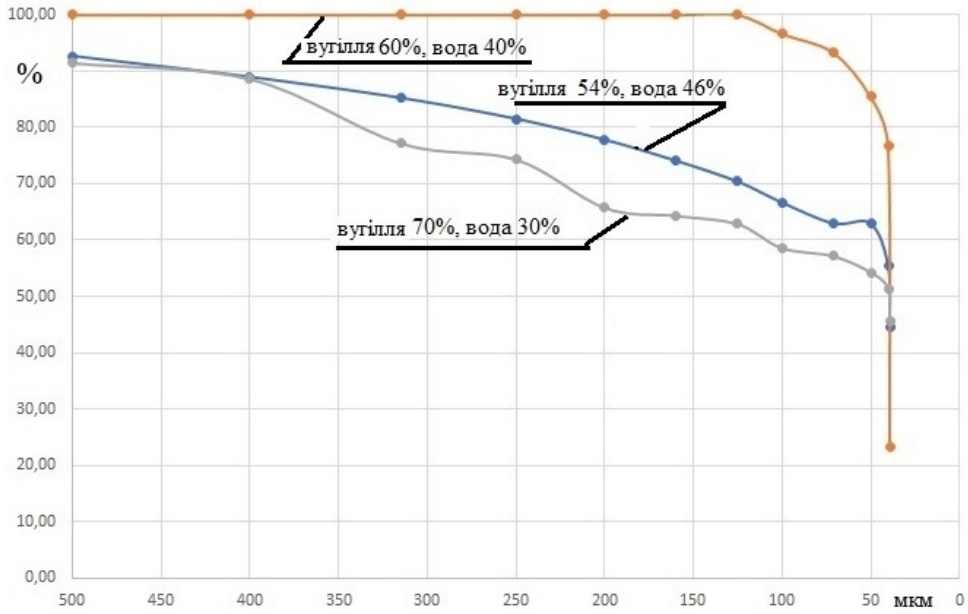


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(3) (4),

$$R_{\%}(i) + R_{\%}(i) + R_{\%}(i-1) = 100, \quad (5)$$

$R_{\%}(i) -$

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); $R_{\%}(i) -$

; $R_{\%}(i-1) -$

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1. : , 1959. 429 . -
 2. : : -
 3. : , 2019. 73 . .
 4. , 2011. 476 . . -
 - 2012. 7 . -
- URL: <https://cyberleninka.ru/article/n/sovremennye-metody-opredeleniya-granulometricheskogo-sostava-poroshkoobraznyh-komponentov-svarochnyh-materialov/viewer>.
5. « » , 2012, 672 . .

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